

2/15/05

astro 731 - Bolometry

I Bolometers vs. Heterodyne Systems

Bolometers are total power detectors.

characteristic	Heterodyne System	Bolometric System
Processing of Radiation	Coherent Detection (Fields are summed then squared)	Incoherent Detection (fields are squared then summed)
Noise	noise terms add linearly $\Delta T_{sys} \sim \frac{\sum T_i}{\sqrt{\Delta \nu \tau}}$ (radiometer eq.)	noise terms add in quadrature $NEP_{sys} \sim \left[ \sum NEP_i^2 \right]^{1/2}$
Bandwidth	10's of GHz (defined by waveguide)	THz
Throughput	$A\Omega = \lambda^2$	$A\Omega = n\lambda^2$ n # of modes
Quantum Efficiency	$T_{sys} > \frac{h\nu}{k}$ (7.2 K at 150 GHz)	none
RAW <del>Typical</del> System Sensitivity (at 150 GHz)	$NET = \frac{T_{sys}}{\epsilon \sqrt{\Delta \nu \tau}}$ $= 2.8 \text{ mK } \sqrt{s}$ for $\Delta \nu = 415 \text{ GHz}$ $T_{sys} = 60 \text{ K}$ $\epsilon = 10\%$	$NET = \frac{NEP}{dP/dT}$ $= \frac{\sum NEP}{\epsilon \int d\nu A\Omega \frac{dB_\nu}{dT} d\nu f(\nu)}$ $= \frac{4 \times 10^{-17}}{4 \times 10^{-13}}$ $= 100 \mu\text{K } \sqrt{s}$

For current bolometers typical NEP's from ground are  $\sim 10^{-17} \text{ W}/\sqrt{\text{Hz}}$   
 CMBPOL, SPECS, & SAFIR will require detectors with  $\text{NEP} \sim 10^{-21} \text{ W}/\sqrt{\text{Hz}}$ !

But there is no free lunch:

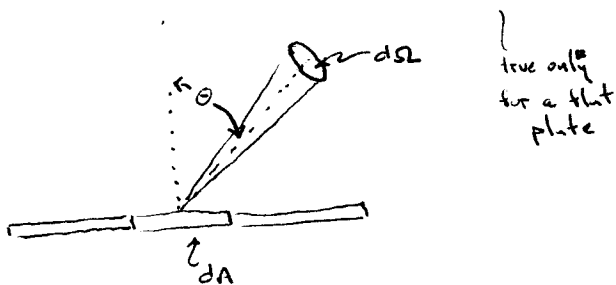
- detectors must be cooled below 300mK
- detectors have relatively small dynamic range
- detectors are microphonically sensitive and very sensitive to RFI
- current bolometers remain complex, fragile, & temperamental

## II The Physics of Bolometers

### A) Optical Model of Simple Bolometer

in general: The infinitesimal power  $dW$  from a solid angle  $d\Omega$  of the sky incident on a surface of area  $dA$  is

$$dW = B \cos\theta d\Omega dA dv$$



true only for a flat plate

$B$  = sky brightness at  $dW$  in  $\frac{\text{W}}{\text{m}^2 \text{Hz sr}}$

$\theta$  = angle between  $d\Omega$  and normal to  $dA$

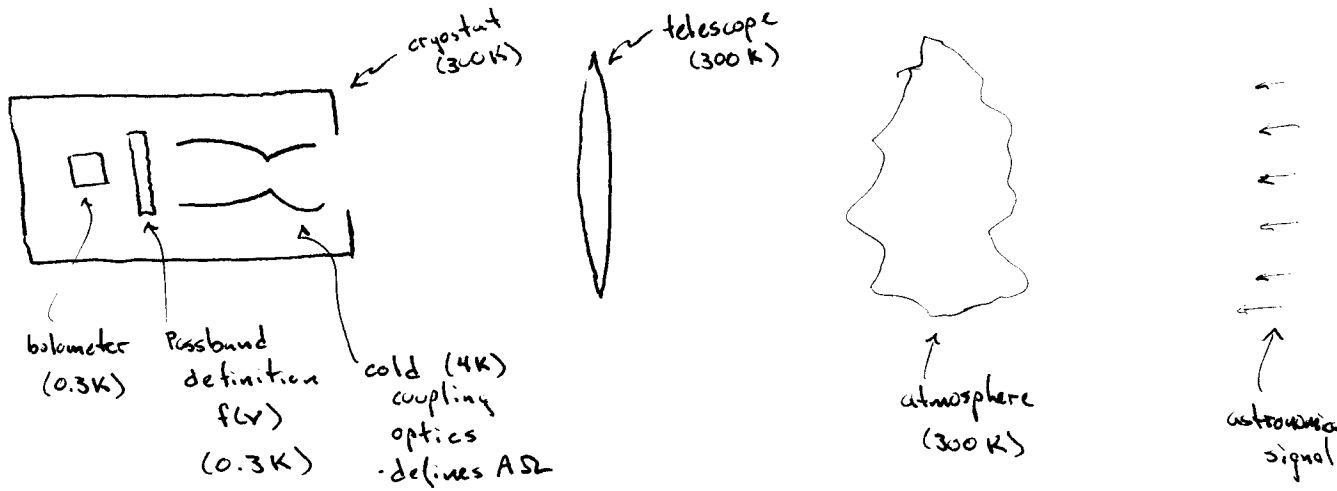
$dv$  = infinitesimal bandwidth in Hz

We design our system such that  $dW$  is uniform across bolometer area  $A$ .  
 Then the power absorbed due to a blackbody with emissivity  $\epsilon$  is

$$W = \epsilon A \int_0^\infty f(\nu) d\nu \int_{\text{sky}} d\Omega P(\theta, \phi) B_\nu(T(\theta, \phi)) \epsilon(\theta, \phi)$$

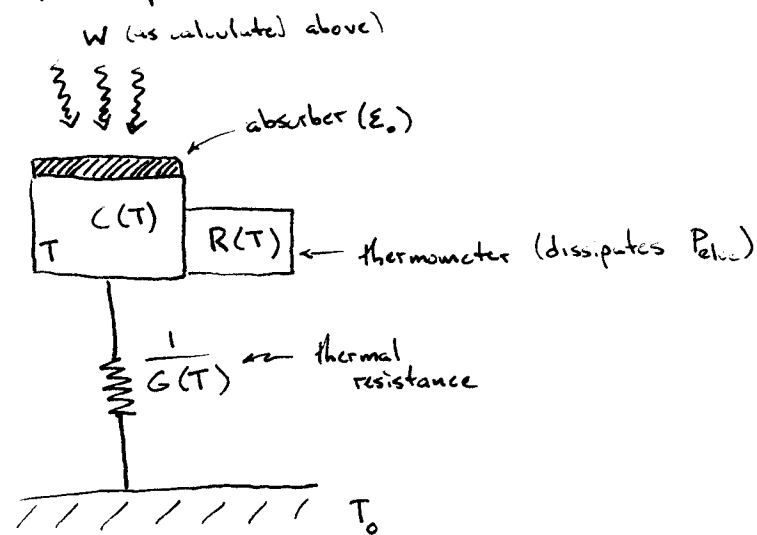
$\uparrow$  spectral bandpass of system (normalized)       $\uparrow$  beam response function (normalized)       $\uparrow$  Planck function       $\uparrow$  emissivity

Of course, a realistic optical system has many sources to consider:



$$W = A \int_0^{\infty} d\nu f(\nu) \int_{\text{sky}} d\Omega P(\theta, \phi) \int_{\epsilon} B_{\nu}(T_i(\theta, \phi)) \epsilon_i(\theta, \phi) \epsilon_i$$

### B) Thermal Model of Simple Bolometer



Power balance:

$$W + P_{elec}(T) = \int_{T_0}^T (G(T) dT) - C(T) \frac{dT}{dt}$$

### c) Electrical Model of Simple Bolometer

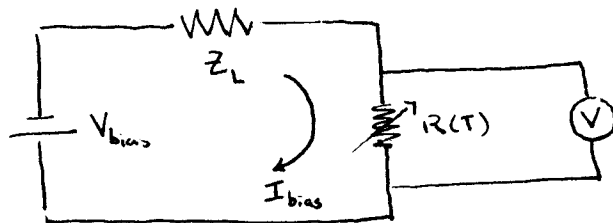
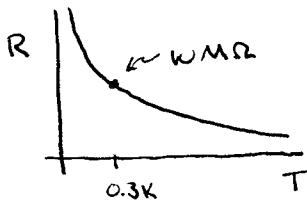
Bolometers typically use a temperature sensitive resistor as the thermometer. There are 2 dominant varieties right now

#### i) $A_2$ TEC Detectors

- thermometer is a doped semiconductor (neutron doped germanium)

$$- R(T) = R_0 e^{\sqrt{T_0/T}}$$

$R_0 \sim 1000 \Omega$   
 $T_0 \sim 25K$



Readout circuit  
(constant current through bolo)

so  $P_{elec} = I_{bias}^2 R(T)$

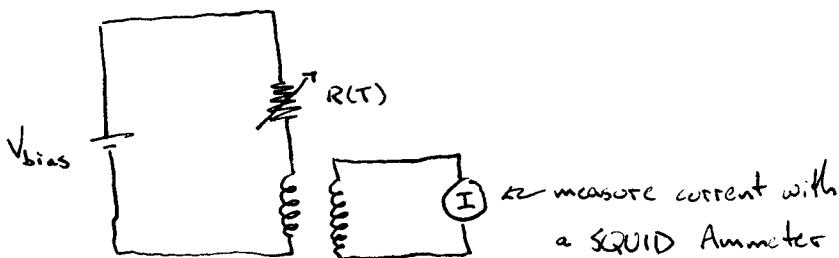
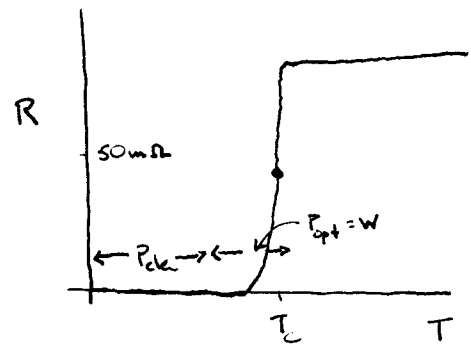
note electrothermal feedback!

#### ii) SPEED Detectors

- thermometer is a superconductor biased into its transition

-  $R = \text{const!}$  (when working)

-  $T = \text{const!}$  (when working)  
 $= T_c$



now  $P_{elec} = \frac{V_{bias}^2}{R}$

↑ strong electrothermal feedback

### III Noise Sources

Three dominant noise sources in bolometers.  
Noise is characterized by the Noise Equivalent Power (NEP).

#### A) Johnson Noise

- fluctuations in internal conductivity of a resistor

$$NEP_{\text{Johnson}} = \sqrt{4kT P_{\text{has}}} \left| \frac{Z_1 + R}{Z_1 - R} \right| (1 + \omega^2 \tau^2)$$

↑ detector time constant =  $\frac{C(T)}{G(T)}$

#### B) Phonon Noise (Thermal Noise)

- shot noise in # of energy carriers in weak thermal link

$$NEP_{\text{phonon}} = \sqrt{4k \bar{G} T^2}$$

↑ temperature weighted average conductivity

#### C) Photon (shot) Noise

- shot noise in # of photons absorbed

$$NEP_{\text{photon}} = \left[ \frac{4A\Omega}{c^2} \frac{(kT_*)^5}{h^3} \int \frac{x^4 dx}{e^x - 1} \left( 1 + \frac{\epsilon_0 \epsilon f(\nu)}{e^x - 1} \right) \epsilon_0 \epsilon f(\nu) \right]^{1/2}$$

where  $x = \frac{h\nu}{kT_*}$

$T_*$  = source temperature

$\epsilon$  = source emissivity

$$NEP_{\text{sys}}^2 = NEP_{\text{Johnson}}^2 + NEP_{\text{thermal}}^2 + NEP_{\text{photon}}^2 + NEP_{\text{electronics}}^2 + \dots$$

↑  
should be the  
dominant term for  
ground-based observations

if  $NEP_{sys} \approx NEP_{photon}$ :

then signal  $\propto$  # of modes (remember that  $A\Omega = n\lambda^2$  for bolometers)  
 while noise  $\propto$  [# of modes]<sup>1/2</sup>

$$\text{so } S/N \propto n^{1/2}$$

also signal  $\propto$  optical efficiency  
 noise  $\propto$  [optical efficiency]<sup>1/2</sup> (over a range of efficiencies)

$$\text{so } S/N \propto \epsilon^{1/2}$$

Why is this important? Because for a  $\sqrt{2}$  increase in  $S/N$  we get a factor of 2 reduction in observing time.

#### IV Map Making with Bolometers

The time-stream signal from a bolometer is composed of a true sky (astronomical + atmosphere) signal + noise. For a particular time  $i$

$$d^i = s^i + n^i \\ = A_{\alpha}^i T^{\alpha} + n^i$$

where  $A_{\alpha}^i = (N_{\text{time ordered data}} \times N_{\text{pixel}})$  matrix

with  $A_{\alpha}^i = 1$  if bolometer sees pixel  $\alpha$  in sample  $i$   
 and  $= 0$  otherwise

$T^{\alpha} =$  temp of sky in pixel  $\alpha$

If the noise is gaussian then it is completely described by  $N^{ij} = \langle n_i n_j \rangle$

and we can write

$$\chi^2 = (d^i - A_{\alpha}^i T^{\alpha}) \underbrace{W_{ij}}_{N^{-1}} (d^j - A_{\alpha}^j T^{\alpha})$$

The best estimator of  $T^{\alpha}$  occurs when  $\frac{\delta \chi^2}{\delta T^{\alpha}} = 0$

this gives

$$T^{\alpha} = \underbrace{(A_{\alpha}^k W_{kl} A_{\beta}^l)^{-1}}_{C^{\alpha\beta}} A_{\beta}^i W_{ij} d_{\beta}^j$$

where  $W_{ij} = N^{-1}$

$\uparrow$  pixel-pixel covariance matrix

Note: while this is the minimum variance solution

- 1) Atmospheric fluctuations are included in  $T^x$
- 2)  $N^{ij}$  is an  $N_{\text{tod}} \times N_{\text{tod}}$  matrix and can not be inverted directly to get  $W$
- 3) No guarantee that noise is gaussian!

The Solution Most Often USED (SCUBA, BOLOCAM)

- assume  $N^{ij}$  is diagonal - every sample is independent.

Note - this is patently untrue.

The Solution We Will Use

- use quadrature channel to insure gaussianity of noise
- use iterative fitting to find best fit  $T^x$  using all bolometers simultaneously.

But that's another lecture...